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TITLE OF INVENTION

GOLF CLUB HEAD

APPLICANT(S) FOR DO/EO/US

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Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39 (1).
4. ☐ A proper Demand for International Preliminary Examination was made by the 19<sup>th</sup> month from the earliest claimed priority date
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2))
- a. ☐ is transmitted herewith (required only if not transmitted by the International Bureau).
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6. ☒ A translation of the International Application into English (35 U.S.C. 371(c)(3)).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(2)).
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- d. ☒ have not been made and will not be made.
8. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☒ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. ☐ A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11. to 16. below concern document(s) or information included:

11. ☒ An Information Disclosure Statement under 37 CFR 1.97 and 1.98./International Search Report
12. ☒ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☒ A FIRST preliminary amendment.  
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14. ☐ A substitute specification.
15. ☐ A change of power of attorney and/or address letter.
16. ☒ Other items or information:

1.) Seven (7) Sheets of Formal Drawings



IN THE U.S. PATENT AND TRADEMARK OFFICE

APPLICANT: Masahide ONUKI et al  
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FOR: GOLF CLUB HEAD

PRELIMINARY AMENDMENT

Assistant Commissioner of Patents  
and Trademarks  
BOX PATENT APPLICATION  
Washington, D.C. 20231

November 23, 1998

Sir:

The following Preliminary Amendments and Remarks are respectfully submitted in connection with the above-identified application.

IN THE SPECIFICATION:

Before line 1, insert --This application is the national phase under 35 U.S.C. §371 of prior PCT International Application No. PCT/JP98/01706 which has an International filing date of April 14, 1998 which designated the United States of America.--

R E M A R K S


The specification has been amended to provide a cross-reference to the previously filed International Application.

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If necessary, the Commissioner is hereby authorized in this, concurrent, and future replies, to charge payment or credit any overpayment to Deposit Account No. 02-2448 for any additional fees required under 37 C.F.R. §1.16 or under 37 C.F.R. §1.17; particularly, extension of time fees.

Respectfully submitted,

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## DESCRIPTION

### GOLF CLUB HEAD

#### TECHNICAL FIELDS

The present invention relates to a golf club head for hitting golf balls.

#### BACKGROUND OF THE INVENTION

Wood type golf club heads for which has been mainly used persimmon have recently turned to be those mainly made of metallic materials such as carbon steel, stainless steel, duralumin, titanium or the like. Such golf club heads can be provided with a larger head volume and a wider hitting face area as well as a larger moment of inertia for obtaining a more stable direction of a golf ball. In addition, a larger sweat area of head is obtainable so as to reduce the lowering of the resiliency of the ball on a miss shot. Moreover, a largersized head of golf club brings about a better stability on addressing as well as permits a longer shaft to be fitted with for obtaining an increased carry.

By the way, the present applicant has obtained an Japanese Patent No.2130519 (No.33071 of Japan Patent Official Gazette of 1993) for a golf club head permitting to increase carry by means of increasing the resiliency performance between the head and golf ball to the full. In said patent, a theory that by means of approaching a frequency indicating the primary minimum of the

mechanical impedance of the head of golf club (hereinafter may be referred to in short as "a primary frequency of the mechanical impedance of head", ) to the frequency indicating the primary minimum of the mechanical impedance of golf ball (hereinafter may be referred simply to as "the primary frequency of the impedance of ball" which proves to be about 600 Hz to about 1600Hz.), the initial speed of impacted ball is raised to the full (hereinafter may be referred to as "the impedance matching theory") has been disclosed.

"Mechanical impedance" is defined as the ratio of the magnitude of a force acting on a point to the responding velocity of another point when said force acted. Namely, when a force applied to an object from outside and the responding velocity are expressed by F and V respectively, the mechanical impedance (Z) is defined as  $Z = F/V$ .

In order to reduce the primary frequency of the impedance of head, it is effective to reduce the rigidity of the hitting face of the head. For example, a larger area of the hitting face, a thinner hitting face, an application of a low Young's modulus material to the hitting face or the like can be cited.

In particular, it is empirically known that, the application of a low Young's modulus metallic material to the hitting face of head renders the feeling (hitting feeling) soft on hitting a golf ball and, favorable to say, even a miss shot hitting transmits only a small shock to hands.

A metallic material with a small tensile strength, even with a low Young's modulus, however, is hard to secure a strength sufficient to endure a shock on impact. Moreover, to enlarge

the thickness of the hitting face for obtaining the strength of the latter resulted only in little effect of reducing the rigidity of said face, which confirmed an existence of a limit also in reducing the primary frequency of the impedance of head.

Also even with a low Young's modulus, a metallic material with a small surface hardness suffers from such problems as the tendency of early wear, easy scratch or the like of the surface of the hitting face due to the friction with ball on impact and sands caught between hitting face and ball on impact.

#### DISCLOSURE OF THE INVENTION

The object of inventions according to claims 1 , 2, 3 or 4 of the present invention is to provide with a golf club head capable of increasing the carry on the basis of the above mentioned "the impedance matching theory" on the basis of the reduction in the rigidity of the hitting face with a strength durable to the shock on impact being secured.

For this sake, a golf club head comprising a hitting face for golf balls, said hitting face formed by a metallic material at least partially, said metallic material satisfying the following relation:

$$y \geq 0.006x + 60$$

wherein, x is Young's modulus(unit: kgf/mm<sup>2</sup>), and y is tensile strength (unit:kgf/mm<sup>2</sup>), is produced. For said metallic material is preferably used an amorphous metal for example. Above all is preferred an amorphous alloy of zirconium base.

Moreover, the object of the inventions according to claims

5 to 8 consists in that on the basis of reduction in rigidity of the hitting face with a hardness being secured, capable of preventing from the wear and the scratch due to the friction with the golf balls on impact and the intervention of sands etc., a golf club head capable of presenting a soft hitting feeling as well as a longer carry is provided on the basis of the impedance matching theory.

For this sake, such a golf club head comprising a hitting face for golf balls, the surface of said hitting face formed by a metallic material at least partially, said metallic material satisfying the following relation:

$$z \geq (x/60) + 200$$

wherein,  $x$  is Young's modulus (unit;  $\text{kgf/mm}^2$ ), and  $z$  is Vickers hardness (unit; HV), is produced. For said metallic material is preferably used an amorphous metal for example. Above all, an amorphous alloy of zirconium base is preferred.

#### BRIEF DESCRIPTION OF DRAWINGS

Fig.1 is a front view of an embodiment of a wood type golf club head,

Fig.2 is a lateral view thereof,

Fig.3 is a cross sectional view of Fig.2,

(A) and (B) of fig.4 are cross sectional views of other embodiments of a golf club head,

Fig.5 is a cross sectional view of head showing another embodiment,

Fig.6 is a front view showing an embodiment of an iron



type golf club head,

Fig.7 is a cross sectional view thereof,

Fig.8 is a graph showing the relation between Young's modulus and tensile strength, and

Fig.9 is a graph showing the relation between Young's modulus and Vickers hardness.

#### THE BEST EMBODIMENT FOR REALIZING THE INVENTION

An embodiment of the present invention will now be explained according to drawings. Fig.1 , Fig.2 and Fig.3 illustrate a golf club head according to the present invention in the form of a hollow wood type golf club head formed by a metallic material. In this example, the head comprises a head body 1 and a face plate 2 arranged in front of the head body 1. And, it is preferable that the golf club head is provided with a head volume of, for example, about 80 cm<sup>3</sup> to about 360 cm<sup>3</sup>, and more preferably of about 230 cm<sup>3</sup> to about 360 cm<sup>3</sup>.

The head body 1 is provided with a face mounting part 1a constituting a periphery of a hitting face 6 for golf balls and permitting to fix thereon the face plate 2, a sole 7 adjoining the face mounting part 1a, a crown part 8 and a side part 9. The face mounting part 1a is represented, for example, in the form in which is formed an opening 3 for fitting bored through into the head which is provided with a stepped down zone 3a for attaching the face plate 2 as shown in Fig.3.

Moreover, the face plate 2, which comprises the main part of the hitting face 6 in the present example, is disposed into

said opening 3 for fitting by a joining means such as welding, caulking and adhesive so as to constitute the hitting face 6 in cooperation with the face mounting part 1a.

The face mounting part 1a may also be formed in the form of an opening 3 without the stepped down zone 3a as shown in Fig.4(A) and also in the form of a tapered concave zone 4 for fitting which widens toward inside of the head and permit to support the back of the face plate 2 as shown in Fig.4 (B). In this case, it is preferable for the face plate 2 also to be made in the nearly same tapered form.

In addition, it was cleared as a result of various experiments made by inventors that it is preferable that part of the hitting face 6 is formed by a metallic material satisfying the following relation:

$$y \geq 0.006x + 60$$

wherein

x is Young's modulus(unit: kgf/mm<sup>2</sup>), and

y is tensile strength(unit: kgf/mm<sup>2</sup>).

The present embodiment illustrates the face plate 2 which is formed by such metallic material as part of the hitting face 6. Consequently, part of the hitting face 6 (in the present example, the face plate 2 comprising the main portion of the hitting face 6) is capable of keeping its Young's modulus low with a tensile strength durable to the shock on impact being secured. Accordingly, the golf club head permits to reduce the primary frequency of the impedance of head and to increase the carry of the golf ball according to said impedance matching theory or to provide with a soft feeling of hitting by reducing

the shock on impact.

In addition, the golf club head permits to keep its tensile strength high with its Young's modulus being maintained low, which may be produced a lighter head by means of applying a smaller thickness for the hitting face 6 or the face plate 2. And also, for example, the smaller the thickness of the face plate 2 becomes, the more the spring constant of head is reduced, resulting in obtaining the more reduced primary frequency of the impedance of head.

Moreover, in the present example, the face plate 2 is shown as having nearly uniform thickness. The thickness of the face plate 2 is preferably, for example, about 1 mm to about 4 mm, and more preferably to be about 1mm to about 3 mm. The eventual thickness of the face plate 2 less than 1 mm tends to have a reduced strength and on the contrary, the eventual thickness more than 4 mm tends to have a less effect of the reduction of the primary frequency of said impedance of the head and the weight thereof.

By the way, the primary frequency of the impedance of golf ball ranges from about 600 Hz to about 1600 Hz, that of ordinary two-piece ball ranging from about 1000 Hz to about 1200 Hz. In contrast therewith, primary frequencies of the impedance of wood type head formed of conventional stainless steel and of that made of titanium are about 1800 Hz to about 2500 Hz and about 1400 Hz to about 2000 Hz respectively.

A golf club head according to the present embodiment permits to obtain a primary frequency of the impedance of head less than that of conventional head and to approximate or coincide same to the primary frequency of the impedance of the

golf ball.

For example, the present embodiment permitted the primary frequency of the impedance of head to be less than 1300 Hz. This is a value substantially coincide with that of two piece ball. Consequently, the golf club head of the present embodiment permits to raise the initial velocity of hit ball on impact to the full, which results in increasing the carry.

Moreover, it is preferable that at least part of the hitting face 6 be formed by a metallic material satisfying the following relation:

$$y \geq 0.006x + 63$$

,and more preferably of a metallic material satisfying the following relation:

$$y \geq 0.006x + 100$$

wherein the definition of x and y is as shown above.

By the way, when the metallic material of the face plate 2, for example, be such that  $y < 0.006x + 60$ , the balance between tensile strength and young's modulus turns worse and it becomes hard to reduce the rigidity of the hitting face with a strength durable to the shock on impact being kept secured.

Moreover, in the present embodiment, the tensile strength of the metallic material of the face plate 2 is preferable to be maintained in such a degree as not increasing the thickness of the face plate 2 remarkably, namely it is preferable to be kept at not less than, for example, 80 kgf/mm<sup>2</sup>, preferably not less than 105 kgf/mm<sup>2</sup> and more preferably not less than 130 kgf/mm<sup>2</sup>. By the way, the upper limit of the tensile strength may be stipulated to be not more than 400 kgf/mm<sup>2</sup> in any combination

with either of above lower limits in consideration of production problems.

Moreover, in the present embodiment the Young's modulus of the metallic material of the face plate 2 is preferable to be not less than, for example, 3000 kgf/mm<sup>2</sup> and preferably not less than 5000 kgf/mm<sup>2</sup>. However, because a too high young's modulus is apt to raise the rigidity of the hitting face 6, so its upper limit is preferable to be not more than 25000 kgf/mm<sup>2</sup> and preferably not more than 20000 kgf/mm<sup>2</sup> and more preferably not more than 16000 kgf/mm<sup>2</sup> and further preferably not more than 12000 kgf/mm<sup>2</sup> and more further preferably not more than 10000 kgf/mm<sup>2</sup> in any combination with either of the lower limits.

While these embodiments were based on lowering the rigidity of the hitting face with a strength durable to shock on impact being secured, a description of such an embodiment as permitting to prevent the surface of the hitting face from wear or scratch caused by the friction with ball on impact or by sands caught between the hitting face and ball shall be followed.

As for the present embodiment also, it is applicable to the golf club head in a form as shown in Figs. 1 to 3 or in Figs. 4 (A), (B). The inventors have found that it is preferable to be formed by such a metallic material as at least part of the surface of the hitting face satisfying the following relation:

$$z \geq (x/60) + 200$$

wherein x is Young' modulus(unit: kgf/mm<sup>2</sup>), and z is Vickers hardness (unit: kgf/mm<sup>2</sup>).

For example, the face plate 2 is formed by metallic material which satisfied the above relation {  $z \geq (x/60) + 200$  }.

By the way, the present example is so comprised that the surface of the face plate 2 is exposed without being provided with any surface layer of other metal, resin, wood or the like.

Moreover, the Vickers hardness of the metallic material is what obtained from relationship between testing load when the testing surface was dented with an indenter of regular square pyramid of diamond with a facing angle of 136 degree and along with the dent surface area, details of which is defined in Japanese-Industrial-Standard (JIS) or the like. The present invention stipulates the testing load as 30 kgf.

In the present embodiment, the face plate 2 can secure a high Vickers hardness so as to prevent the hitting face 6 from wear and scratch caused by the friction with the golf balls and sands caught within. Moreover, the metallic material of the face plate 2, which possesses the above stated relation of Young's modulus  $x$  with Vickers hardness  $z$ , permits to keep the Young's modulus low with a high Vickers hardness being maintained.

Accordingly, the golf club head also of the present embodiment can reduce the primary frequency of the impedance of head, permitting to increase the carry of ball according to the impedance matching theory. In addition, part of the surface of the hitting face, which suffers from a reduced shock on impact because of a lower Young's modulus, provides a softer hitting feeling.

By the way, in the present embodiment, when the face plate 2 is a metallic material of  $z < (x/60) + 200$ , the simultaneous satisfaction of such three performances as softer hitting feeling, increase in carry and durability of hitting face 6 prove

to be unobtainable.

In addition, because the face plate 2 becomes capable of keeping the Vickers hardness high with the Young's modulus being kept low, a reduction in the thickness of the hitting face 6 (face plate 2) is also possible. Accordingly, a lighter head may be produced and the spring constant of head is increased corresponding to the reduction in the thickness of the face plate 2, synergetic effect of which permitting to reduce the more the primary frequency of the impedance of head.

Herein, the Vickers hardness of the face plate 2 is preferable to be not less than 250 HV, and preferably not less than 300 HV, more preferably not less than 370 HV, or further preferably not less than 400 HV be selected, a very excellent injury resistance shall be ideally obtained. Moreover its upper limit may be stipulated as not more than 1000 HV from the view point of production problems or the like, also in a combination with either of said lower limits. The latter permits to obtain a more suitable protection of the hitting face from an injury.

In addition, it is preferable that at least part of the surface of the hitting face 6 is formed by a metallic material satisfying the following relation:

$$z \geq (x/60) + 250$$

wherein the definition of x and z is as shown above.

In the present embodiment too, the Young's modulus of the face plate 2 is preferable to be, for example, not less than 3000 kgf/mm<sup>2</sup> and preferably not less than 5000 kgf/mm<sup>2</sup> for obtaining a required rigidity. However, because a too high Young's modulus is apt to render the rigidity of the hitting face 6 higher, so

its upper limit is desired to be not more than 25000 kgf/mm<sup>2</sup> and preferably not more than 20000 kgf/mm<sup>2</sup> and more preferably not more than 16000 kgf/mm<sup>2</sup> and further preferably not more than 12000 kgf/mm<sup>2</sup>, more further preferably not more than 10000 kgf/mm<sup>2</sup> in combination with either of said lower limits, too.

While said two embodiments were described, for metallic material comprising such face plate 2, it is preferable to use amorphous metal for example. The amorphous metal means a metal whose atomic arrangement is not regular over a wide range. At present it is made mainly in such a manner that a fused alloy obtained by melting various alloy elements is rapidly cooled to solidify so as not crystal nucleus being produced and grown. In the present embodiment, an amorphous metal whose amorphous ratio that is the degree of amorphousness, that is to say, the ratio of the volume  $v_1$  of the amorphous phase to the total volume  $v$ , ( $v_1/v$ ) is over 50% is preferably used.

The amorphous metal consists of composition expressed by a general formula:  $M_a X_b$  (wherein "a" and b are  $65 \leq a \leq 100$  and  $0 \leq b \leq 35$  at atomic %).

Herein, M consists of metallic elements of more than one kind selected from Zr, V, Cr, Mn, Fe, Co, Ni, Cu, Ti, Mo, W, Ca, Li, Mg, Si, Al, Pd, Be, and X consists of metallic elements of more than one kind selected from Y, La, Ce, Sm, Md, Hf, Nb, Ta. And preferably, above "a", b are preferable to be  $99 \leq a \leq 100$  and  $0 \leq b \leq 1$  at atomic % respectively.

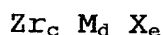
Because such amorphous metals, which may be provided simultaneously with a high tensile strength, a high Vickers hardness and a low Young's modulus, prove to be metallic



materials particularly suitable to the golf club head of the present invention.

And for said amorphous metal, amorphous alloys of zirconium base are more preferably applicable. The zirconium base amorphous metals are provided with a higher tensile strength as well as a lower Young's modulus. In addition, a relatively lower cooling velocity is applicable in production, accordingly, they are practical and preferable also from the view point that by casting molten metal in a mold and cooling same to obtain bulk or plate form products with a relative ease.

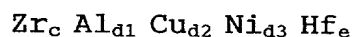
The amorphous zirconium base alloys consist of a composition as shown by a general formula:



(wherein c, d and e are  $20 \leq c \leq 80$ ,  $20 \leq d \leq 80$  and  $0 \leq e \leq 35$  atomic % respectively).

However, Zr is zirconium, M is a metallic element of more than one kind selected from V, Cr, Mn, Fe, Co, Ni, Cu, Ti, Mo, W, Ca, Li, Mg, Si, Al, Pd, Be; and X consists of metallic elements more than one kind, selected from Y, La, Ce, Sm, Nd, Hf, Nb, Ta.

In addition, said c, d and e are preferable to be  $35 \leq c \leq 75$ ,  $25 \leq d \leq 65$  and  $0 \leq e \leq 30$  respectively, more preferably to be  $35 \leq c \leq 75$ ,  $25 \leq d \leq 65$  and  $0 \leq e \leq 1$  at atomic %, and further preferably to be  $50 \leq c \leq 75$ ,  $25 \leq d \leq 50$ ,  $0 \leq e \leq 1$  at atomic % respectively. Moreover, said M is particularly preferable to be Al, Cu, Ni. Said X is preferable to be Hf. In particular, as such a zirconium base amorphous alloy, for example,



is preferable. (herein, shall be  $d1+d2+d3=d$  and  $c+d+e=100$ ).

And, the amorphous metal is preferable to present an amorphous ratio mentioned above of not less than 75%, more preferably not less than 80% and further preferably not less than 90%. For example, such amorphous ratio can be identified by means of observing under an optical microscope to determine the area of amorphous portion after a mirror polishing followed by an etching treatment of a cut section of a sample of metallic material. And the amorphous ratio can be adjusted by modifying the alloy composition of amorphous metal, the cooling temperature of cooling fused alloy for producing an amorphous metal as well as the oxygen concentration of the ambient gases and so on. Above all, the more said cooling velocity is raised and the more the oxygen concentration of the ambient gases is reduced, the more the amorphous ratio can be raised.

By the way, as for the metallic material of the face plate 2, any kind of metallic material such as any alloy or elemental metal other than amorphous metals, so long as it satisfies the relation between said Young's modulus and tensile strength or that between Young's modulus and Vickers hardness, may be applied, without being limited to the illustrated amorphous alloys.

In connection with the present embodiment, various methods permit to change designs. For example, the face plate 2 may be constructed a thicker central part with a periphery part whose thickness reduces gradually to outwardly. In this case, it is possible to obtain the less primary frequency of the impedance of head without reducing the strength of face plate 2. On the contrary, the face plate 2 may be constructed a thinner central part with a periphery part whose thickness gradually

increases to outwardly. In this case, it is preferable because the strength of the joint portion of the face plate 2 with the face mounting part 1a for receiving same is increased.

Moreover, the head body 1 may be formed by conventional metallic materials such as titanium, titanium alloys, stainless steels or the like for example.

And also, as shown in Fig.5, the hitting face 6, the sole 7, the crown part 8 and the side part 9 constituting a head as a whole may be formed by a metallic material satisfying the following relation:

$$y \geq 0.006x + 60$$

wherein the definition of x and y is as shown above, or may be formed by a metallic material satisfying the following relation:

$$z \geq (x/60) + 200$$

wherein the definition of x and z is as shown above. In these case, further improved shock endurance and hitting feeling are obtained, resulting in a further reduction in the primary frequency of the impedance of head.

In Figs.6 and 7, as another embodiment of the present invention, a metallic iron type club head is shown. In this example, it is shown a golf club head which comprises a head body 101 and the insert plate 102 for the hitting face to be fitted on the side of the hitting face 104 of the head body 101. The insert plate 102 for the hitting face comprises the main part of the hitting face 104 to hit the golf ball chiefly on its surface. And the insert plate 102 for the hitting face of the present embodiment is shown formed in substantially uniform thickness as well as fitted in a fitting hollow formed on the side of the

hitting face 104 of head body 101 and fixed by adhesion, welding, caulking, press in etc. Consequently, in this example, the back as a whole of the insert plate 102 for the hitting face comes into contact with or sticks to the head body 101, which results in an improvement of the durability of the hitting face 104.

Moreover, by means of applying for the insert plate 102 for the hitting face, for example, metallic material satisfying the following relation:

$$y \geq 0.006x + 60$$

wherein the definition of x and y is as shown above, or a metallic material satisfying the following relation:

$$z \geq (x/60) + 200$$

wherein the definition of x and z is as shown above, an effect similar to the above mentioned can be obtained.

While several embodiments were above described, although the present invention is preferable for wood type and iron type heads, it is also available for a putter type head.

In addition, in all embodiments above stated, the face plate 2 as well as the insert plate 102 for the hitting face may be formed by a metallic material simultaneously satisfying the following relations:

$$y \geq 0.006x + 60$$

$$z \geq (x/60) + 200$$

wherein the definition x, y and z is as shown above.

In this case, according to the impedance matching theory, such a further preferable golf club head is produced as possessing a strength durable to the shock on impact and a face with a very high durability hard to be injured, simultaneously

with an improvement in carry of ball.

#### WORKING EXAMPLE

(First Working example)

Wood type golf heads were produced (examples 1 to 6) with zirconium base amorphous alloys with variously varied alloy elements (Zr-Al-Cu-Ni-Hf, or Zr-Al-Cu-Ni) being applied to part of the hitting face. These golf club heads were used to investigate head speed, ball speed after hitting by the golf club head, resilience coefficient, carry (hitting distance from the hitting point to first dropping point of golf ball), total hitting distance, primary minimum frequency of the mechanical impedance of head and hitting feeling. The results were reported in Table 1. On the other hand, for comparison, references 1 and 2 were given wherein wood type hollow heads made of titanium and stainless steel were prepared for comparing several performances. The head speed, the ball speed, the resilience coefficient, the carry and the total hitting distance were determined by the hitting test by a golf swing robot. For measuring the primary minimum frequency of the mechanical impedance of the head was utilized an exciting measuring method wherein a vibration exciter, an acceleration pickup, a power unit, and a dynamic signal analyzer same as those utilized in said Japanese patent. Moreover, the hitting feeling was evaluated by 20 golfers who actually hit and effected 5 steps of 1 to 5 points of sensuous evaluation on the basis of less shock, (whether or not being obtained a soft hitting feeling) for obtaining its mean value.

As clear from Table 1, while primary minimum frequencies of mechanical impedance of golf club heads in references 1 and 2 are 1450 Hz and 1980 Hz respectively, in examples, all frequencies are held below 1290 Hz. Accordingly, golf club heads in all examples obtained primary minimum frequencies of the mechanical impedance of heads less than those of conventional heads and it was confirmed that they approximated to the primary minimum frequency of the mechanical impedance of two piece ball (about 1000 Hz to about 1200 Hz). By the way, illustrated tensile strengths of metallic materials applied to the face plate were below 200 kgf/mm<sup>2</sup>.

Moreover it is clear that resilience coefficient, carry, total hitting distance are all superior with examples to those with references 1 and 2. In addition as for hitting feeling also, that of examples 1 to 6 is superior to that of references 1 and 2.

In these examples, the thickness of the face plate (amorphous metal part) is set the smaller with increasing tensile strength. It is considered that this decrease in thickness further lowers the spring constant as regards the hitting face, which resulted in an increase in restitution coefficient, carry, and total hitting distance and an improvement in hitting feeling.

Moreover, Fig.8 shows the relation between Young's modulus  $x$  and tensile strength  $y$ . For metallic materials used for face plates of above mentioned examples 1 to 6 and references 1 and 2, were made plottings on Fig.8. Equally for data of duralumin, magnesium alloys, and super high tensile strength steels were shown plottings likewise.

In Fig.8, straight lines 10, 11 and 12 are graphs showing  $y=0.006x+60$ ,  $y=0.006x+63$ , and  $y=0.006x+100$  respectively. Herein, a range satisfying,  $y \geq 0.006x+60$  is indicated by oblique lines.

It is clear that while metallic materials used in examples satisfy  $y \geq 0.006x+60$ , with materials used in references and with duralumin, magnesium alloy, super high tensile strength steels etc.,  $y < 0.006x+60$  is satisfied.

#### (Second Working Example)

Next, as another working example of the present invention, a relation between Young's modulus and Vickers hardness was investigated. Heads of iron type similar to what was shown in Figs.6 and 7 (examples 7 to 9) and of wood type similar to what was shown in Figs. 1 to 3 (examples 10 to 12) were produced. Moreover, iron type heads (references 4 to 6) and wood type ones (references 7 to 9) whose insert plates for hitting face and face plates were made of stainless steel, titanium, or duralumin were produced. And as for these heads, tests were made chiefly in connection with the injury resistance of the surface of the hitting face and the softness of hitting feeling.

The injury resistance of the surface of the hitting face was determined in such a manner that a golf ball placed on the ground was hit by a golf swing robot so as to let intervene a small amount of sands between the ball and the surface to examine the amount of injury on the surface of the hitting face. On the other hand, the softness of hitting feeling was evaluated by 20 golfers to adopt mean value of its results. And measuring load

for Vickers hardness is of 30 kgf. Results of test are shown in Tables 2 and 3.

As clear from Tables 2 and 3, as for club heads of all examples, the surface of the hitting face is hard to be injured (little injured or very little injured) and presents a soft hitting feeling (good or very good). And, at least either of performances of the injury of the hitting face and the soft feeling resulted in very good.

Moreover, the example 7 gives a Vickers hardness similar to that of references 3, 4 (similar injury resistance) but its Young's modulus is very lowered. Accordingly it can be understood that the golf club head of this example permits to increase carry and provide with a soft hitting feeling on the one hand, it suffers little from injury from sands and pebbles on the other hand, presenting an excellent wear resistance.

And, Fig.9 shows a relation between Young's modulus  $x$  and Vickers hardness  $z$  of metallic materials. The data of said metallic materials of face plates of examples 7 to 9 and references 3 to 8 and also of magnesium and super high tensile strength steels being plotted.

In said figure, straight lines 16 and 17 indicate  $z=(x/60)+200$  and  $z=(x/60)+250$  respectively. Moreover a range satisfying a relation  $z \geq (x/60)+200$  is shown by oblique lines. As clear from said figure, examples 7 to 12 satisfy the relation  $z \geq (x/60)+200$ .

As described above, the golf club head according to the claim 1 permits part of the hitting face to be provided with a lower rigidity with a tensile strength durable to shock on



impact being maintained. Accordingly, a golf club head with a less primary minimum frequency of the mechanical impedance of head than that of conventional golf club head is produced. For example, the value of the primary minimum frequency of the mechanical impedance of golf club head may be further approached that of golf ball. Consequently, a longer carry as well as softer hitting feeling may be obtained. Moreover, as for the golf club head, the thickness of its hitting face may be reduced and further reduction in weight may be attempted. And when the thickness of the hitting face was reduced, by an amount corresponding thereto the spring constant of the hitting face is reduced and moreover the primary minimum frequency of the mechanical impedance may be reduced.

And, with the golf club head according to the claim 2, for a metallic material suitable to said hitting face an amorphous metal is applied, which permits to obtain with ease a compromise between a high tensile strength and a low Young's modulus.

And with a golf club head according to the claim 3 or 4, an amorphous alloy of zirconium base is applied, which permits its simple production and in addition the compromise between a higher tensile strength and a lower Young's modulus.

And, with a golf club head according to the claim 5, at least part of the surface of the hitting face can be made so as to keep its low rigidity with its surface hardness durable to a friction and a sand intervention on impact being maintained. Accordingly, a primary minimum frequency of the mechanical impedance less than that of the conventional golf club is

available with the durability and injury resistance of head being maintained. For example, the primary minimum frequency of the mechanical impedance of golf club head may be further approximated to that of golf ball. Accordingly, an increased carry as well as a softer hitting feeling at hitting is obtained. Moreover, a smaller thickness of the hitting face of the golf club head may be obtained, which means a further reduced weight being obtainable. In addition, a reduction in the thickness of the hitting face induces a reduction in the spring constant by its corresponding amount and in addition permits to further reduce the primary minimum frequency of the mechanical impedance.

With the golf club head according to the claim 6, an application of an amorphous metal as a metallic material suitable to said hitting face permits to achieve with ease a compromise of a high tensile strength with a low Young's modulus.

Moreover, the golf club head according to the claim 7 or 8, for which is applied an amorphous alloy of zirconium base, may be made in a simpler manner and in addition, a compatibility of a higher tensile strength with a lower Young's modulus may be attainable.

TABLE 1

	Ex. 1	Ex. 2	Ex. 3	Ex. 4	Ex. 5	Ex. 6	Ref. 1	Ref. 2
Head speed Vh(m/s)	41.02	41.27	41.21	41.13	41.09	41.24	41.38	41.30
Ball speed Vb(m/s)	58.66	58.85	59.59	59.27	59.13	59.51	58.84	58.48
Resilience coefficient	1.430	1.426	1.445	1.441	1.439	1.443	1.422	1.416
Carry (m)	210.8	210.1	216.2	213.2	212.9	214.9	207.6	206.5
Total distance (m)	232.4	229.5	238.2	235.0	234.7	237.1	228.4	223.7
Face plate								
Material	Anorphous alloy of zirconium base	Anorphous alloy of zirconium base	Anorphous alloy of zirconium base	Anorphous alloy of zirconium base	Anorphous alloy of zirconium base	Anorphous alloy of zirconium base	Titanium	Stainless steel
Composition (Atomic %)								
Zr	54	64	55	55	60	55		
Al	10	10	10	10	10	10		
Cu	30	15	30	30	20	30		
Ni	5	10	5	5	10	5		
Hf	1	1	--	--	--	--		
Anorphous ratio (%)	57	82	96	77	82	80	11600	20800
Young's modulus x (kgf/mm <sup>2</sup> )	7000	16000	6500	5000	10000	5000		
Tensile strength y (kgf/mm <sup>2</sup> )	105	160	175	130	160	130	120	134
Thickness (mm)	3.4 (Uniformly)	2.5 (Uniformly)	2.4 (Uniformly)	3.0 (Uniformly)	2.8 (Uniformly)	3.0/2.5 in center/On periphery	3.2 (Uniformly)	3.2 (Uniformly)
Primary minimum frequency of the mechanical impedance of the hitting face (Hz)	1260	1290	960	1130	1120	1080	1450	1980
Hitting feeling	3.75	3.25	5.00	4.50	4.25	5.00	3.00	2.25

Resilience coefficient: (Vb/Vh)

TABLE 2

	Ex.7	Ex.8	Ex.9	Ref.3	Ref.4	Ref.5
Insert plate for hitting face						
Material	Amorphous alloy of zirconium base	Amorphous alloy of zirconium base	Amorphous alloy of zirconium base	Stainless steel	Titanium	duralumin
Composition (Atomic %)						
Zr	55	64	55			
Al	10	10	10			
Cu	25	15	30			
Ni	10	10	5			
Hf	--	1	--			
Amorphous ratio (%)	76	81	93			
Young's modulus x (kgf/mm <sup>2</sup> )	7200	15000	6500	20800	11600	7000
Vickers hardness z (HV)	370	500	500	370	360	140
Thickness (mm)	3.0	3.0	3.0	3.0	3.0	3.0
Injury on the hitting face	little	very little	very little	little	little	many
Soft feeling performance	very good	good	very good	bad	good	very good

TABLE 3

Face plate	Ex. 10	Ex. 11	Ex. 12	Ref. 6	Ref. 7	Ref. 8
Material	Amorphous alloy of zirconium base	Amorphous alloy of zirconium base	Amorphous alloy of zirconium base	Stainless steel	Titanium	duralumin
Composition (Atomic %)						
Zr	55	64	55			
Al	10	10	10			
Cu	25	15	30			
Ni	10	10	5			
Hf	--	1	--			
Amorphous ratio (%)	75	79	94			
Young's modulus x (kgf/mm <sup>2</sup> )	7200	15000	6500	20800	11600	7000
Vickers hardness z (HV)	370	500	500	370	360	140
Thickness (mm)	3.4	2.9	2.4	3.2	3.0	4.5
Injury on the hitting face	little	very little	very little	little	little	many
Soft feeling performance	very good	good	very good	bad	good	very good

## CLAIMS

1. A golf club head comprising a hitting face for golf balls, said hitting face formed by a metallic material at least partially,

said metallic material satisfying the following relation:

$$y \geq 0.006x + 60$$

wherein

x is Young's modulus(unit: kgf/mm<sup>2</sup>), and

y is tensile strength(unit: kgf/mm<sup>2</sup>).

2. A golf club head according to the claim 1, wherein said metallic material is amorphous metal.

3. A golf club head according to the claim 1, wherein said metallic material is amorphous alloy of zirconium base.

4. A golf club head according to the claim 1, wherein said metallic material is amorphous alloy comprising Zr, Al, Cu, Ni, Hf or said amorphous alloy comprising Zr, Al, Cu, Ni.

5. A golf club head comprising a hitting face for golf balls, the surface of said hitting face formed by a metallic material at least partially,

said metallic material satisfying the following relation:

$$z \geq (x/60) + 200$$

wherein

x is Young's modulus(unit: kgf/mm<sup>2</sup>), and

z is Vickers hardness(unit: HV).

6. A golf club head according to the claim 5, wherein said metallic material is amorphous metal.

7. A golf club head according to the claim 5, wherein said metallic material is amorphous alloy of zirconium base.

8. A golf club head according to the claim 5, wherein said metallic material is amorphous alloy comprising Zr, Al, Cu, Ni, Hf or said amorphous alloy comprising Zr, Al, Cu, Ni.

## ABSTRACT OF THE INVENTION

A golf club head comprising a hitting face for golf balls, said hitting face formed by a metallic material at least partially, said metallic material satisfying the following relation:

$$y \geq 0.006x + 60$$

wherein

x is Young's modulus(unit: kgf/mm<sup>2</sup>), and

y is tensile strength(unit: kgf/mm<sup>2</sup>). The metallic material is preferable amorphous metal.



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Fig. 1

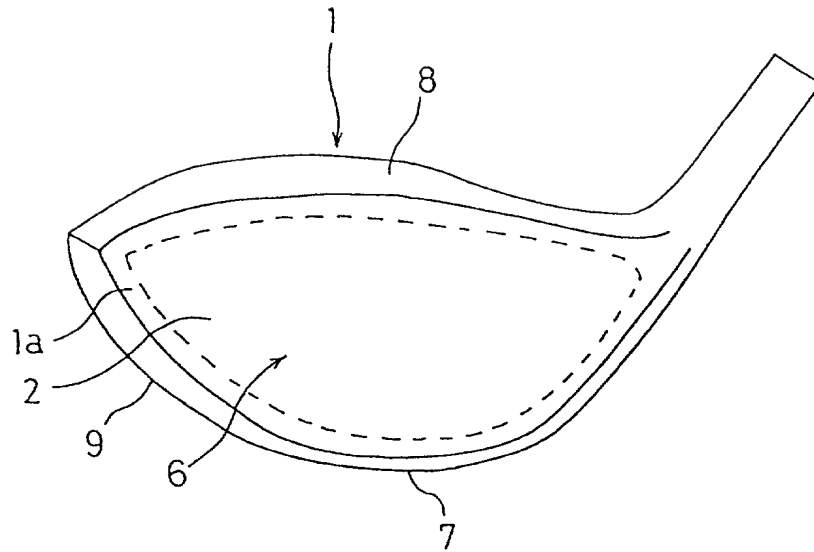


Fig. 2

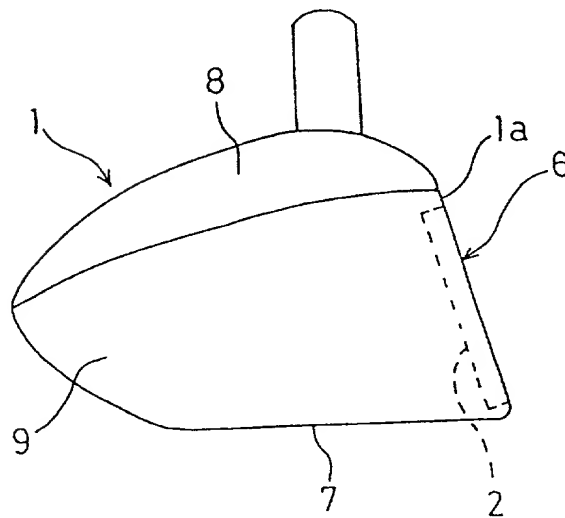


Fig. 3

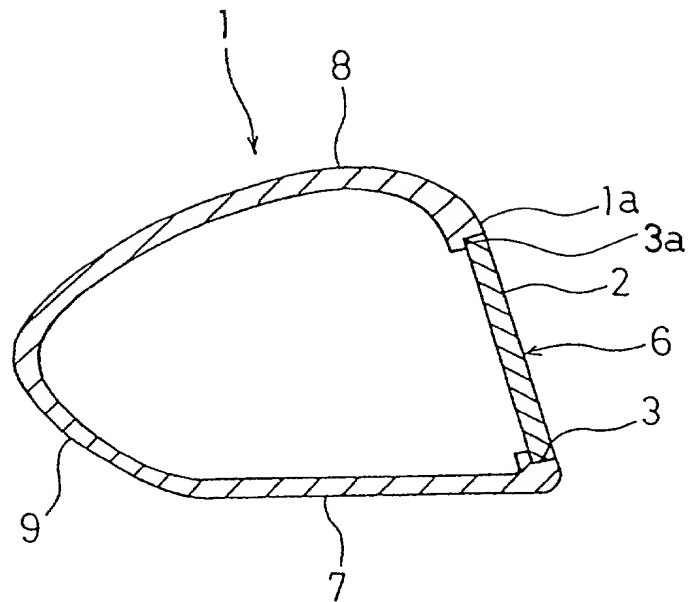
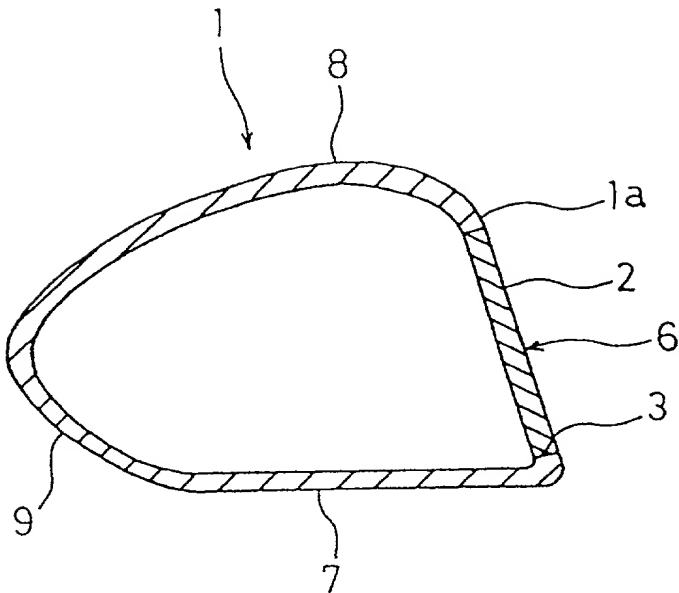


Fig. 4

( A )



( B )

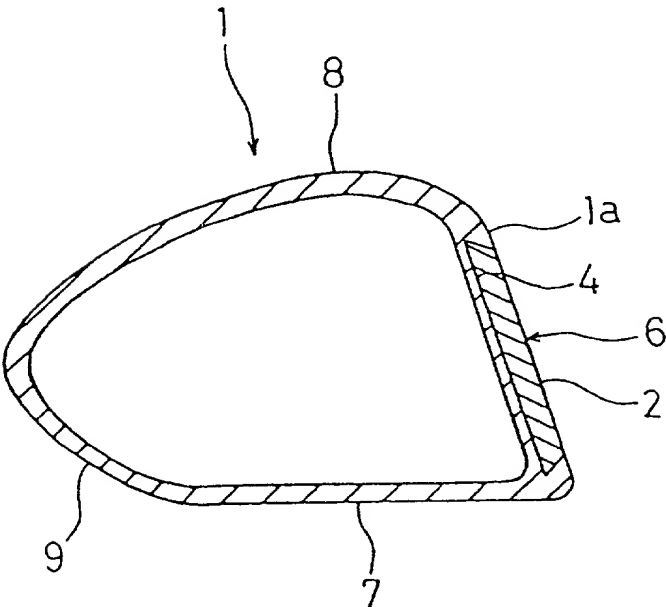
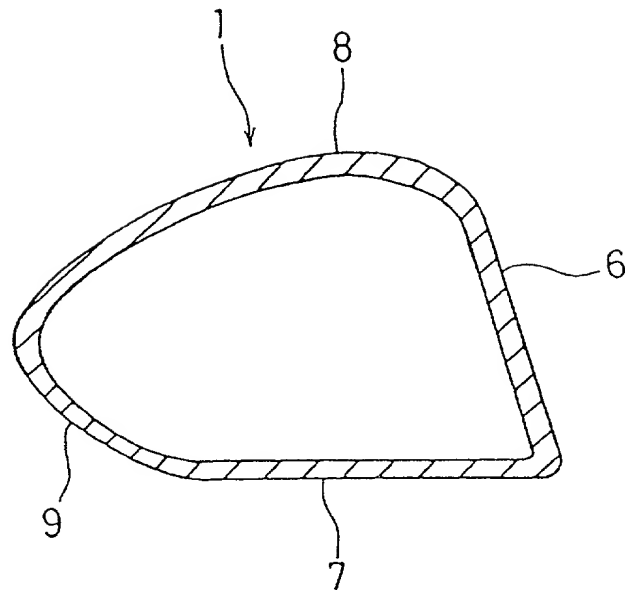


Fig. 5



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Fig. 6

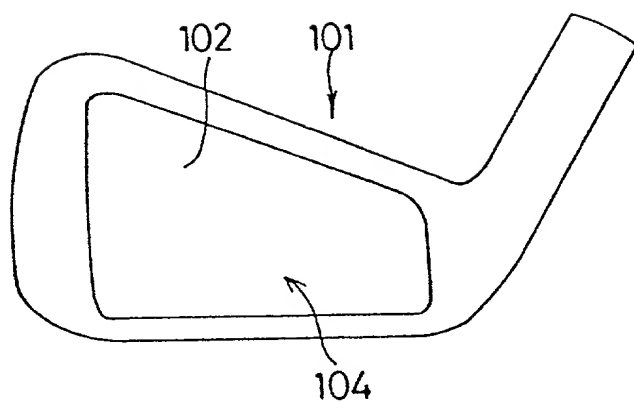
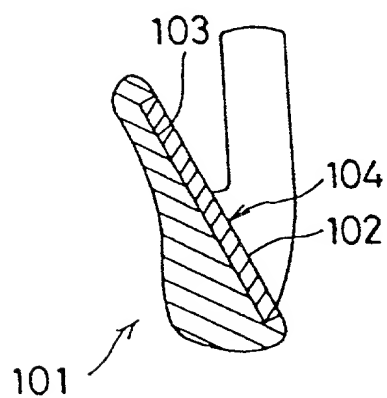
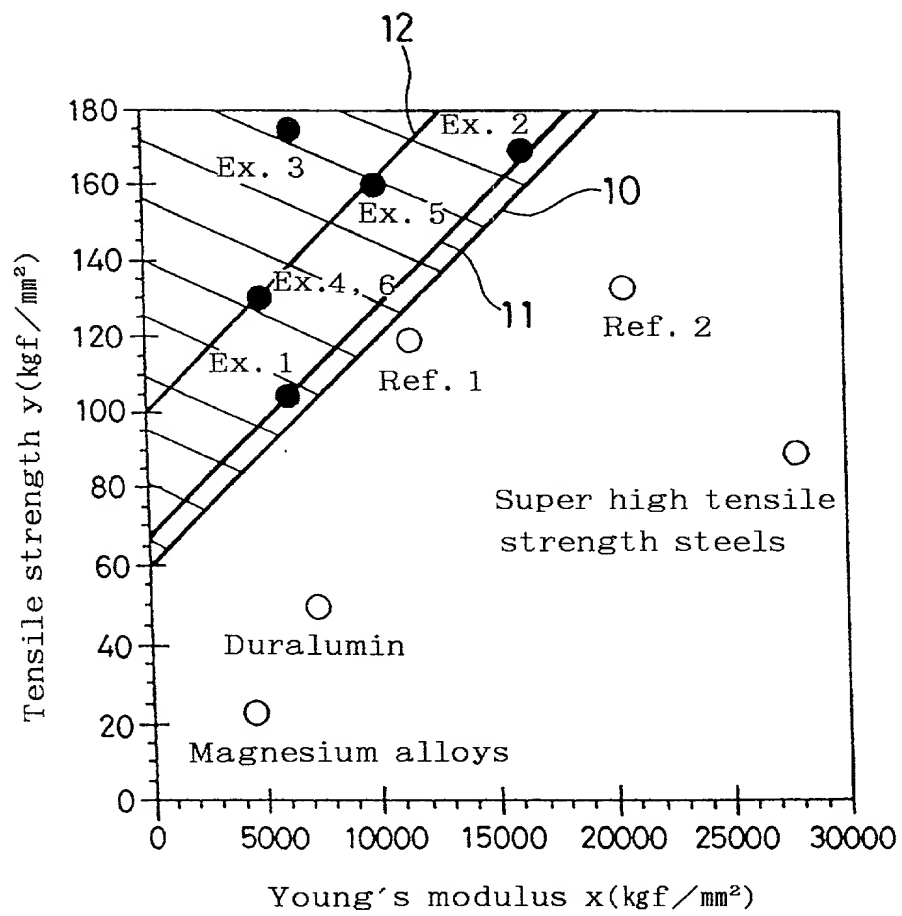


Fig. 7



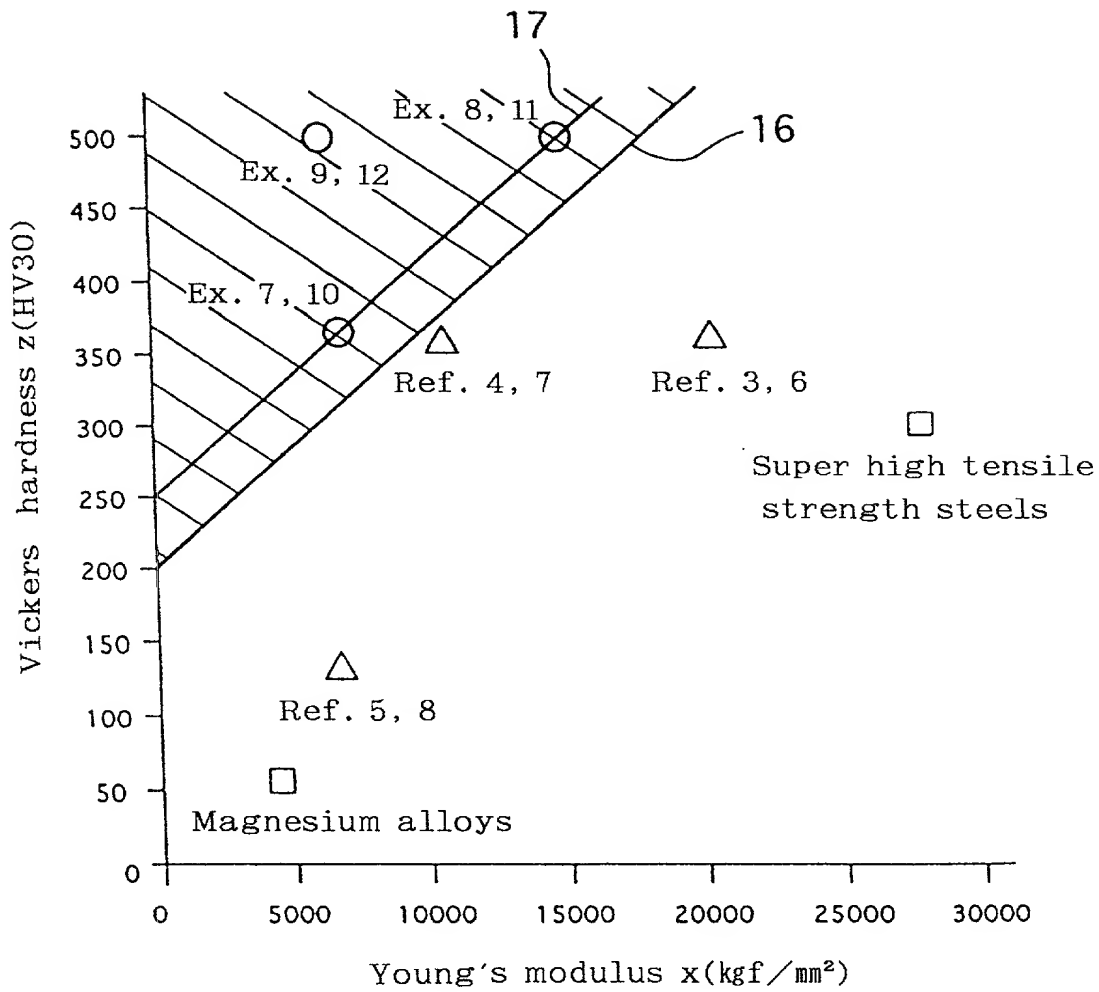
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Fig. 8



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Fig. 9



# BIRCH, STEWART, KOLASCH & BIRCH, LLP

## COMBINED DECLARATION AND POWER OF ATTORNEY FOR PATENT AND DESIGN APPLICATIONS

ATTORNEY DOCKET NO.

229-532P

As a below named inventor, I hereby declare that: my residence, post office address and citizenship are as stated next to my name; that I verily believe that I am the original, first and sole inventor ( if only one inventor is named below) or an original, first and joint inventor (if plural inventors are named below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

### GOLF CLUB HEAD

the specification of which is attached hereto. If not attached hereto,

the specification was filed on \_\_\_\_\_ as  
United States Application Number \_\_\_\_\_ ; and/or  
the specification was filed on \_\_\_\_\_ as PCT  
International Application Number \_\_\_\_\_ ; and was  
amended under PCT Article 19 on \_\_\_\_\_ (if applicable)

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, § 1.56.

I do not know and do not believe the same was ever known or used in the United States of America before my or our invention thereof, or patented or described in any printed publication in any country before my or our invention thereof or more than one year prior to this application, that the same was not in public use or on sale in the United States of America more than one year prior to this application, that the invention has not been patented or made the subject of an inventor's certificate issued before the date of this application in any country foreign to the United States of America on an application filed by me or my legal representatives or assigns more than twelve months (six months for designs) prior to this application, and that no application for patent or inventor's certificate on this invention has been filed in any country foreign to the United States of America prior to this application by me or my legal representatives or assigns, except as follows.

I hereby claim foreign priority benefits under Title 35, United States Code, § 119 (a)-(d) of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

#### Prior Foreign Application (s)

			Priority Claimed	
9-115316	Japan	April/16/1997	<input checked="" type="checkbox"/>	<input type="checkbox"/>
(Number)	(Country)	(Month/Day/Year Filed)	Yes	No
9-147219	Japan	May/20/1997	<input checked="" type="checkbox"/>	<input type="checkbox"/>
(Number)	(Country)	(Month/Day/Year Filed)	Yes	No
			<input type="checkbox"/>	<input type="checkbox"/>
(Number)	(Country)	(Month/Day/Year Filed)	Yes	No

I hereby claim the benefit under Title 35, United States Code, § 119(e) of any United States provisional application (s) listed below.

(Application Number)

(Filing Date)

All Foreign Applications, if any, for any Patent or Inventor's Certificate Filed More Than 12 Months (6 Months for Designs) Prior To The Filing Date of This Application:

Country

Application No.

Date of Filing (Month/Day/Year)

I hereby claim the benefit under Title 35, United States Code, § 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, § 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, § 1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application:

(Application Number)

(Filing Date)

(Status - patented, pending, abandoned)



I hereby appoint the following attorneys to prosecute this application and/or an international application based on this application and to transact all business in the Patent and Trademark Office connected therewith and in connection with the resulting patent based on instructions received from the entity who first sent the application papers to the attorneys identified below, unless the inventor(s) or assignee provides said attorneys with a written notice to the contrary:

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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